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**AGH UNIVERSITY OF SCIENCE
AND TECHNOLOGY**



**Electric-field controlled
spintronic devices (E-CONTROL)**

Micromagnetic analysis of voltage-driven dynamics in thin ferromagnetic layer systems

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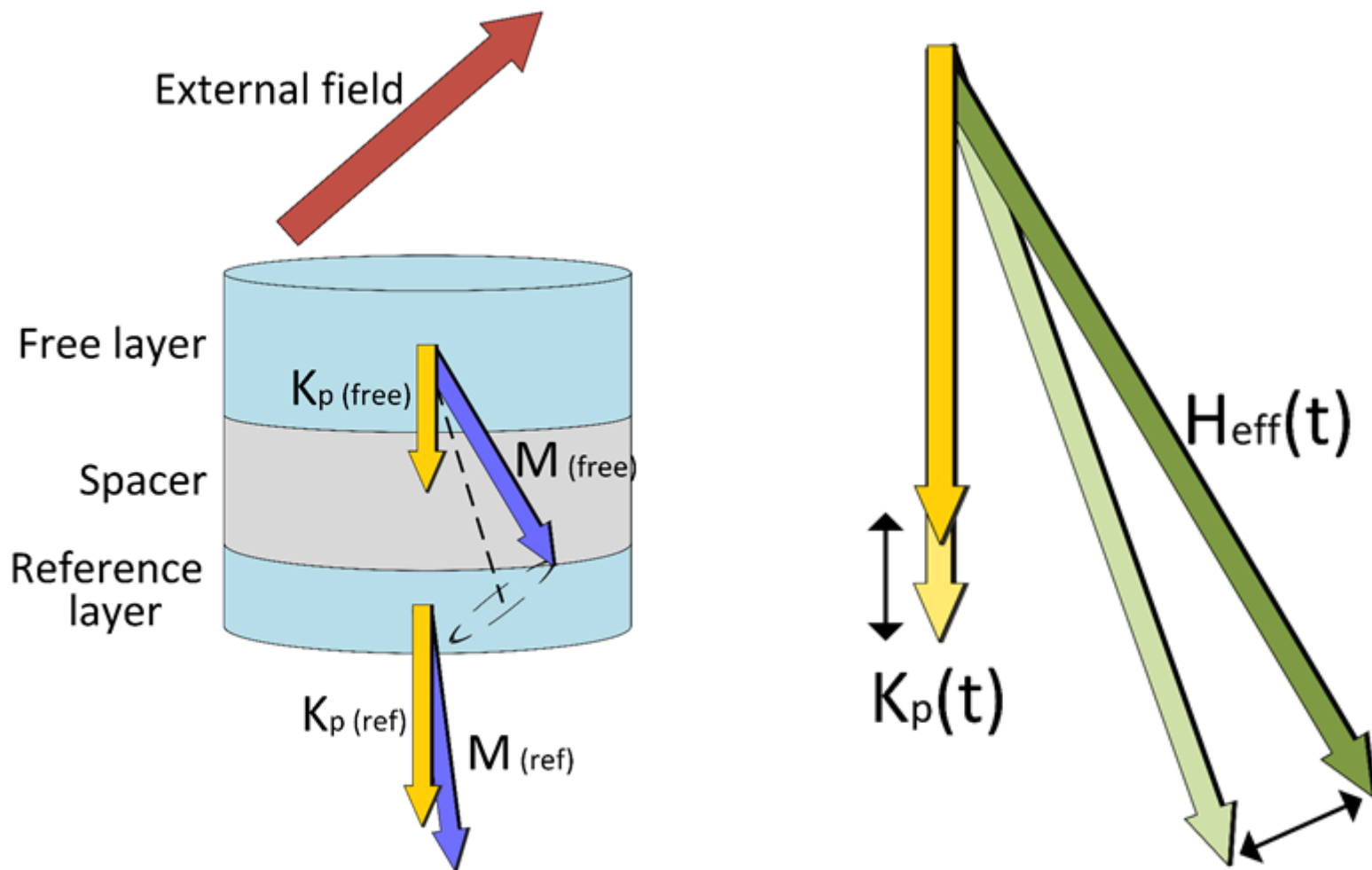
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Outline

- Introduction to voltage-driven dynamics
- Effective anisotropy
- Approach and sample used
- Voltage-induced switching
- FMR lineshape
- Simulation results for different anisotropy regimes
- Summary and acknowledgements

Magnetization equilibrium manipulation



Voltage-driven dynamics

Junction with thick tunnel barrier
> 1.5 nm

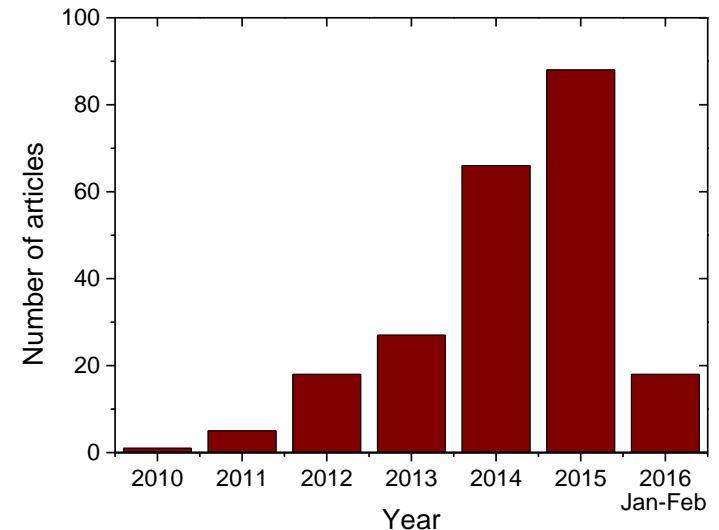


High resistance of the device

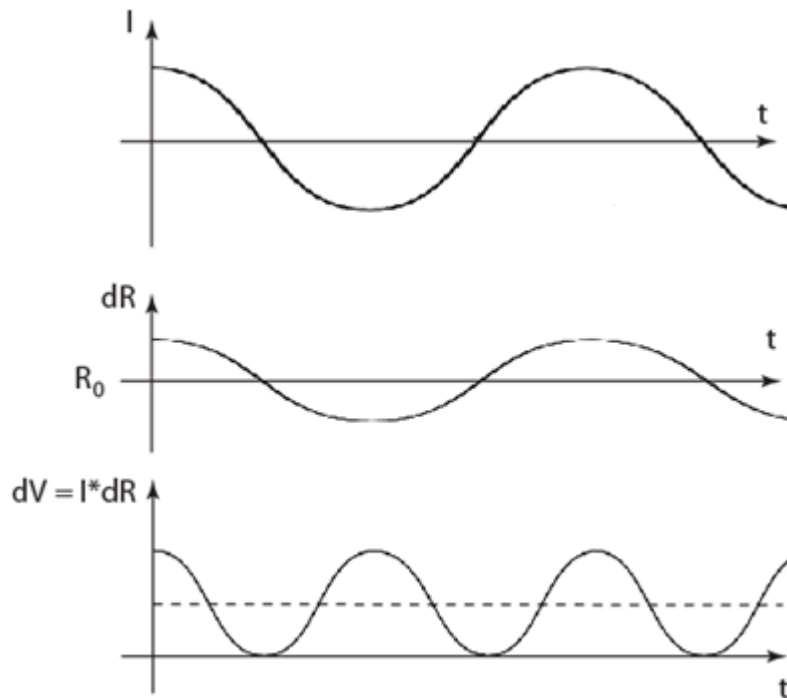


Negligible current in comparison
to current-controlled devices

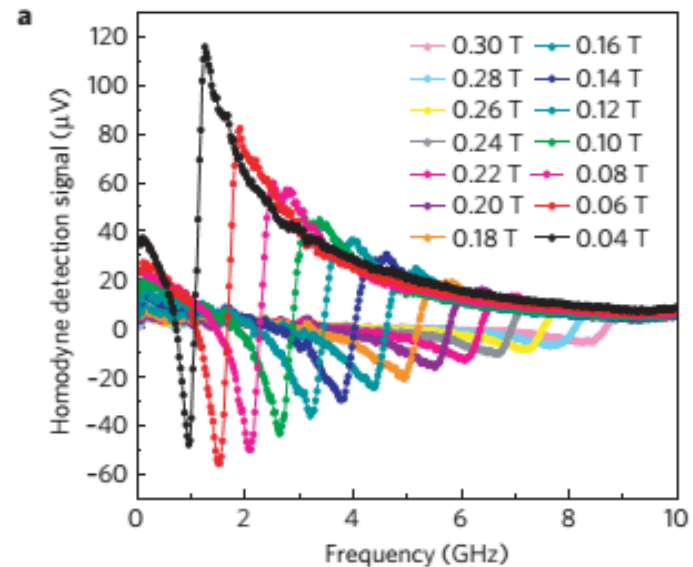
**AC voltage control
of anisotropy desired
for low energy
consumption
applications**



Detection via spin diode effect



- MTJ supplied with radio frequency signal
- Precession of magnetization in phase with input signal – mixing results in a DC signal generation



Tulapurkar et al. Nature 438, 339, 2005

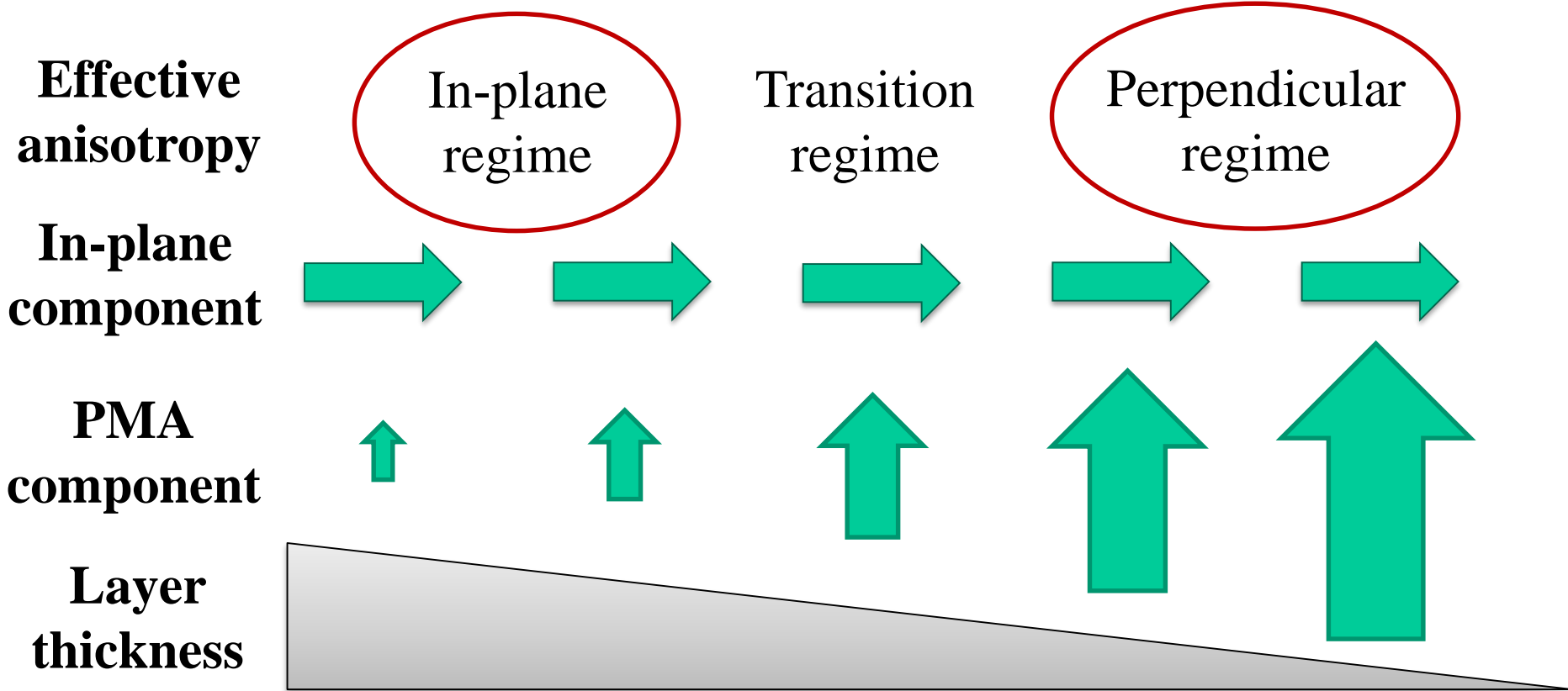
Nozaki et al. Nature Phys 8, 491, 2012

PMA vs. in-plane anisotropy

Recently reported:

Skowroński et. al., APEX 8.5 (2015): 053003

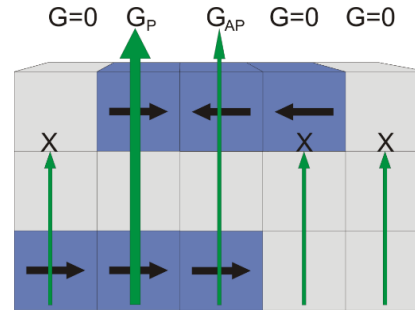
Commonly investigated
in literature



Micromagnetic approach

OOMMF-based simulations

$$\frac{d\vec{m}}{dt} = -\gamma_0 \vec{m} \times \vec{H}_{eff} + \alpha \vec{m} \times \frac{\partial \vec{m}}{\partial t}$$



*M.J. Donahue, D.G. Porter,
NIST Report (1999).
M. Frankowski et. al.
Phys. B 435, 105–108 (2014).*

Ferromagnetic free layer: 1.4 nm (2 cells), M_s 1200 kA/m, K out-of-plane VARIABLE kJ/m³

MgO barrier: 1.4 nm (2 cells)

Ferromagnetic reference layer: 0.7 nm (1 cell), M_s 1000 kA/m, K out-of-plane 1500 kJ/m³

- Custom OOMMF extension installed on the PL-Grid infrastructure
- Intrinsic (Gilbert) damping constant 0.017
- Alternating anisotropy contributes to the effective field H_{eff}

Calculations of lineshape

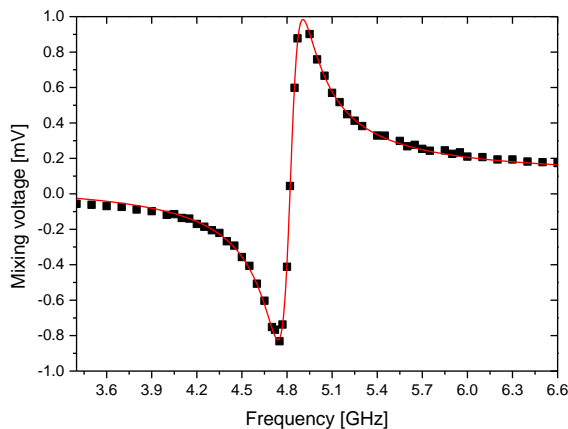
Resonance frequency calculations for different external field values

50-100 simulations for a single set of parameters generated automatically

Parallel computations give raw simulation result

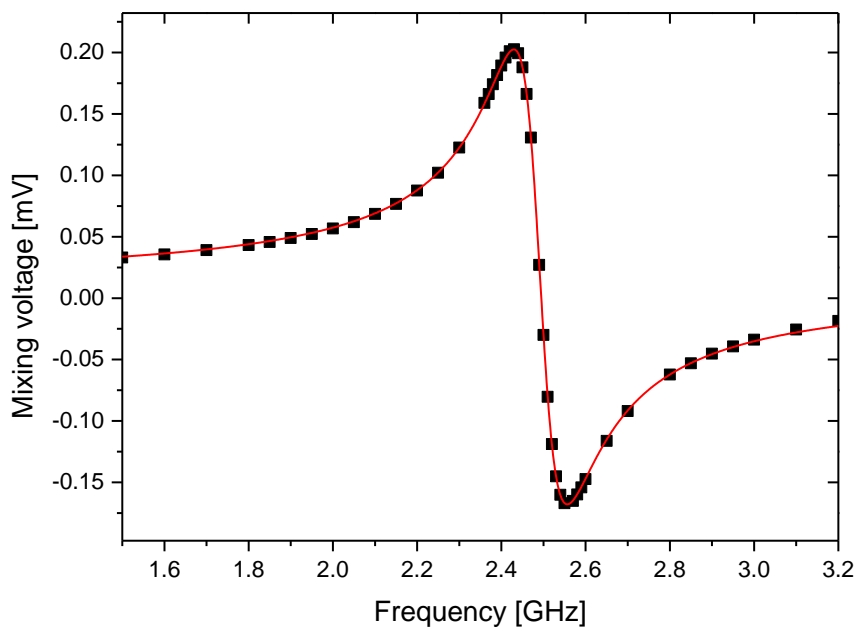
Post-processing to obtain the final lineshape

f_1
 f_2
...
 f_r
...
 f_{n-1}
 f_n

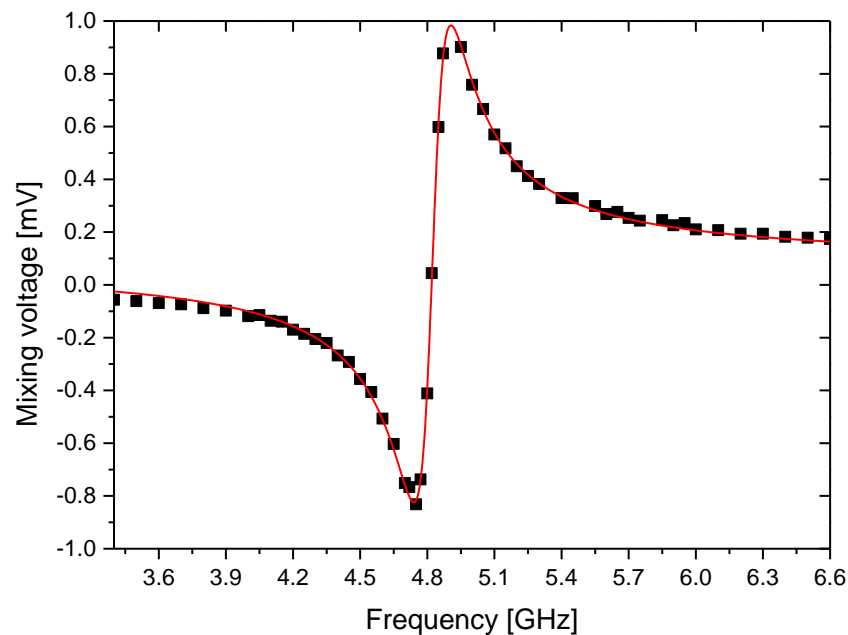


Calculations of lineshape

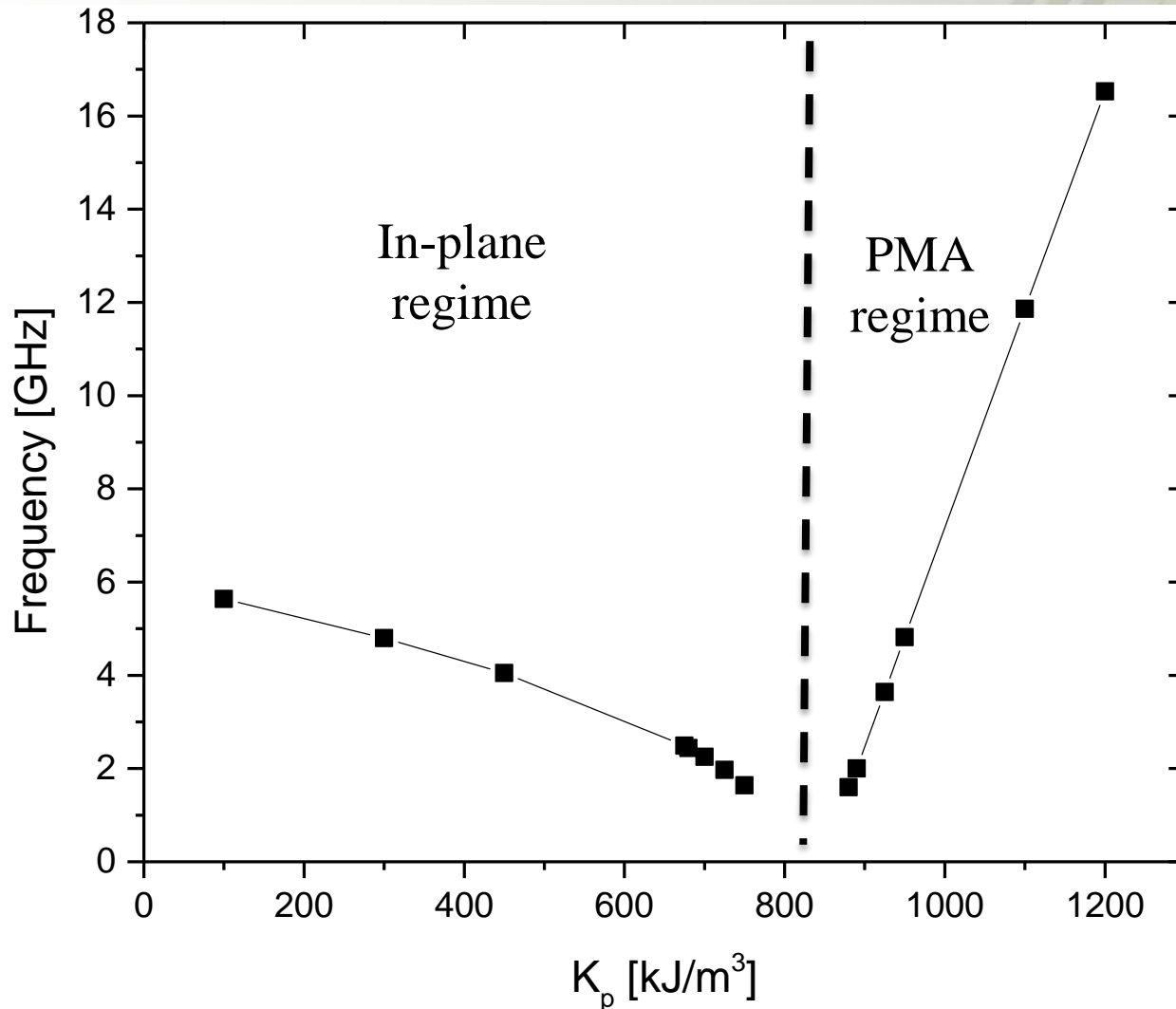
$K_p = 675 \text{ kJ/m}^3$
 $K_{\text{effective}} : \text{in-plane}$



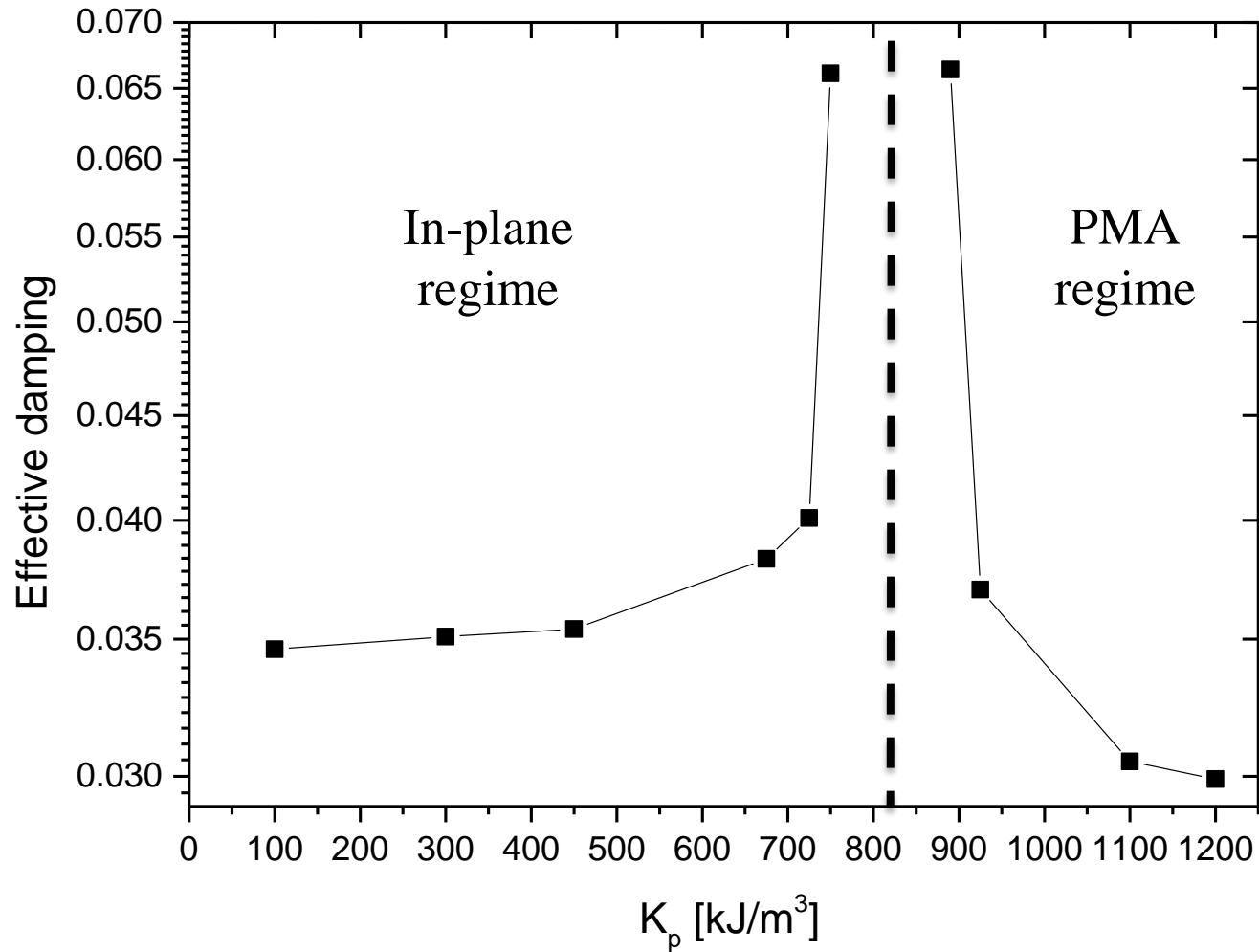
$K_p = 950 \text{ kJ/m}^3$
 $K_{\text{effective}} : \text{PMA}$



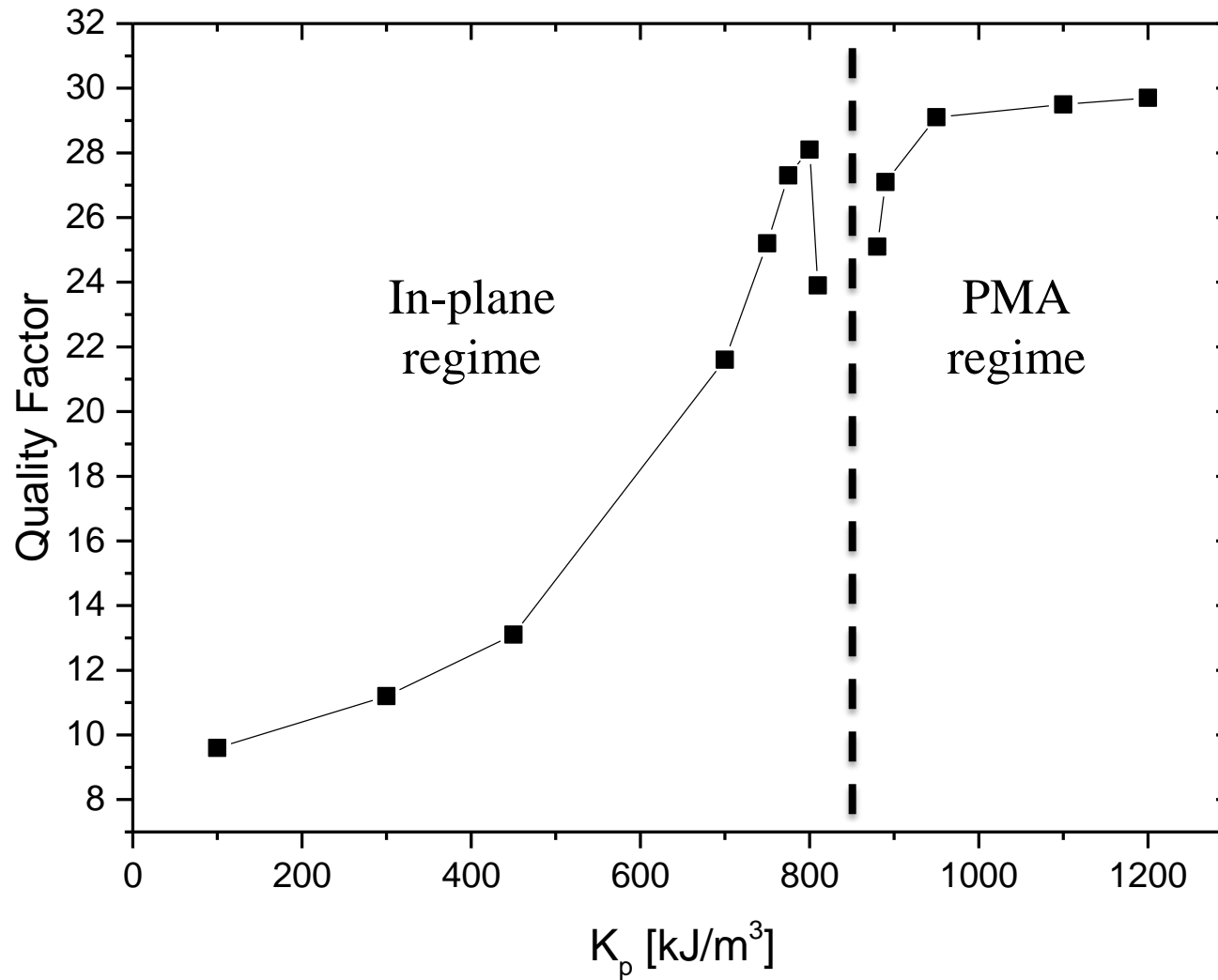
Frequency



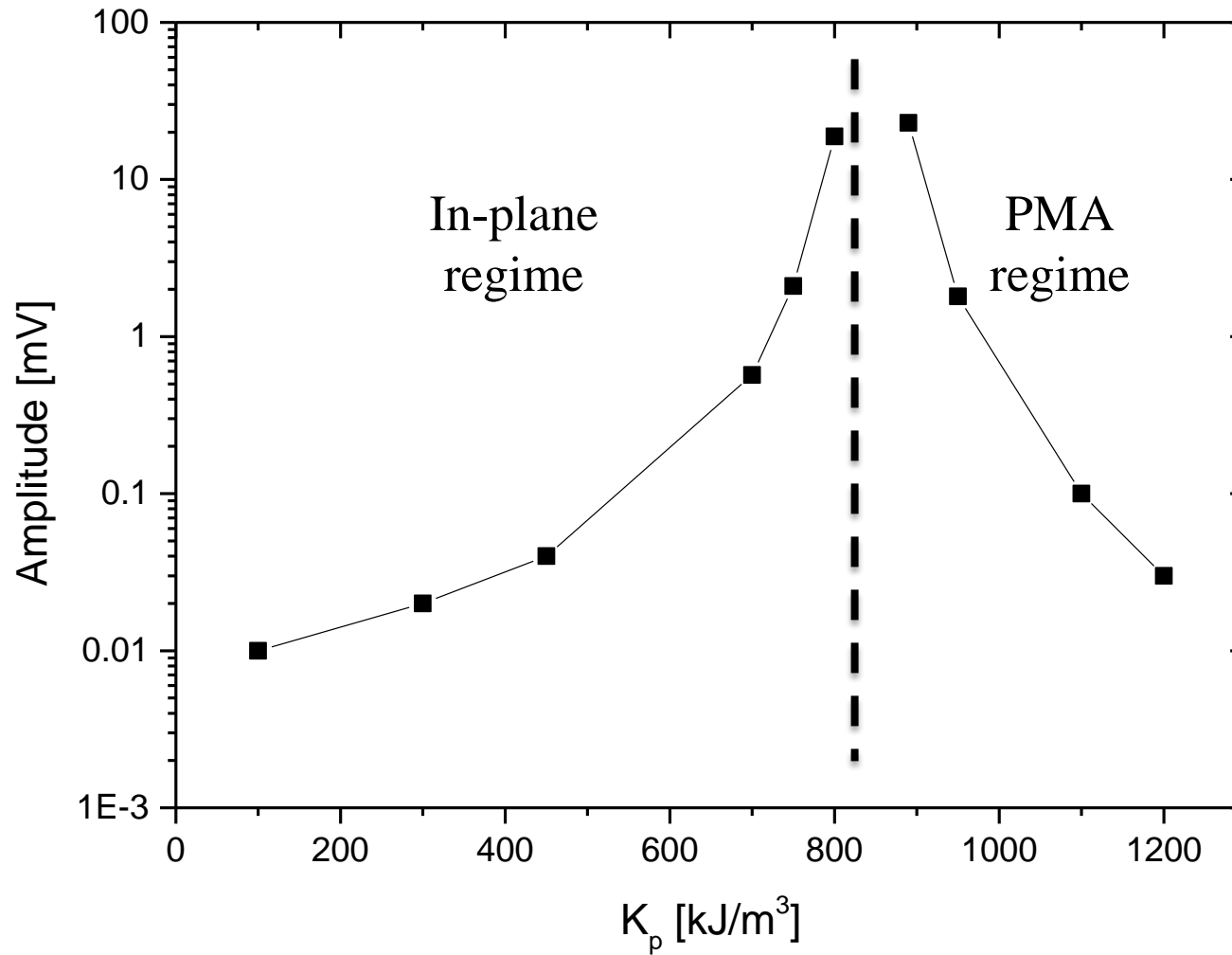
Effective damping



Quality factor



Peak-to-peak amplitude



Summary

- Our approach allows for modelling of voltage-induced spin-diode effect and ferromagnetic resonance lineshape
- Both in-plane and PMA anisotropy regimes are characterized by antisymmetric lineshape
- We find that the amplitude of oscillations and effective damping increase as the effective anisotropy moves towards the transition point.
- The quality factor is the largest in the case of a strong perpendicular anisotropy, but the amplitude of the response is very low in this regime



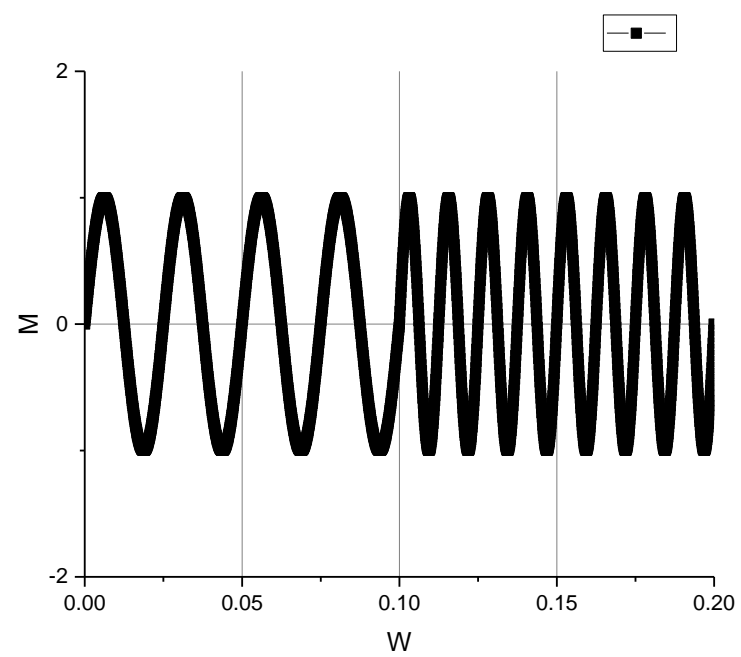
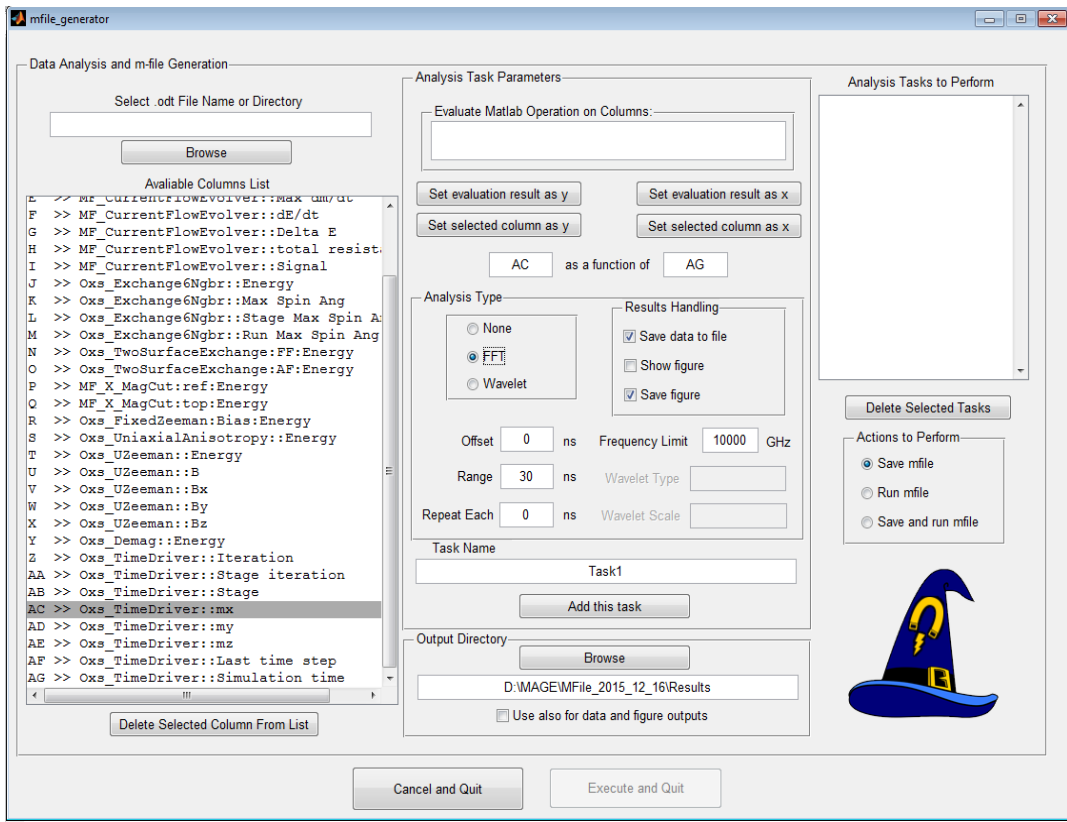
Acknowledgements

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- Numerical calculations were supported by the PL-Grid infrastructure.
- J.Ch. acknowledges the scholarship under Marian Smoluchowski Krakow Research Consortium KNOW programme.

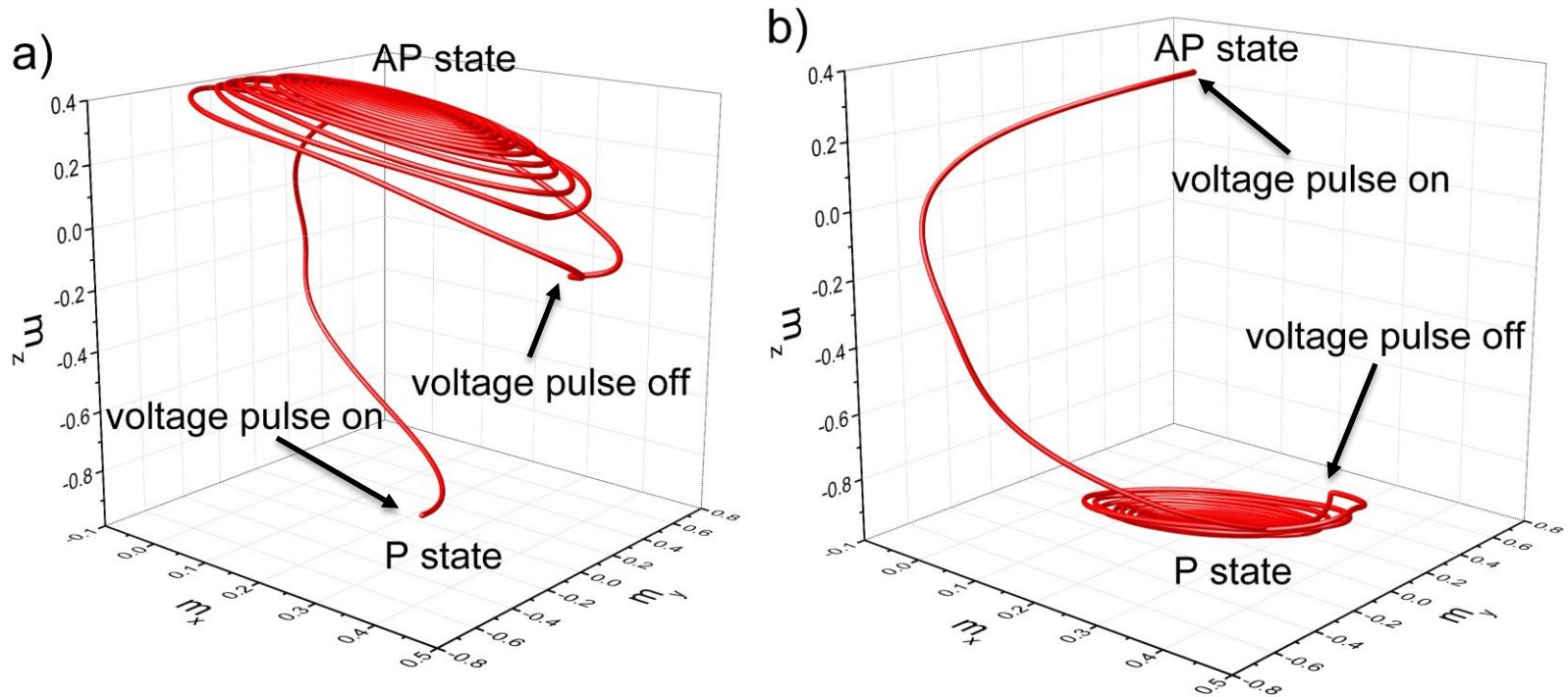


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Appendix: custom software



Appendix: voltage-induced switching



Magnetization trajectories for voltage-induced switching, single pulse (duration of 0.55 ns) and amplitude 100 kJ/m^3 , field bias 40 mT 45° to sample plane



Appendix: how is the effective damping calculated?

$$\alpha_{eff} = \frac{\sqrt{3}\Delta f_{pp}}{\frac{\gamma}{2\pi}(H_1+H_2)}, \text{ where}$$

$$H_1 = (H_{ext} + H_{ref})\sin(\theta_H - \theta_M) - H_d \sin^2 \theta_M$$

$$H_2 = (H_{ext} + H_{ref})\sin(\theta_H - \theta_M) + H_d \cos 2\theta_M$$

are fitted from the $f = \frac{\gamma}{2\pi} \sqrt{H_1 H_2}$ relationship,

and Δf_{pp} is obtained from fitting the antisymmetric Lorentz formula to the simulated lineshape.

based on: *Nozaki, Takayuki, et al., APEX 7.7 (2014): 073002.*